

b.) Amendments to the Specification:

Please amend the specification on page 80, lines 7-19 to read as follows:

--Examples of the mechanical impact application apparatus may include: mechanical pulverizers, such as ~~KRYOPRON~~ "KRYPRON SYSTEM" (made by Kawasaki Jukogyo K.K.) and "TURBOMILL" (made by Turbo Kogyo K.K.), and mechanical impacting devices, such as "MECHANOFUSION SYSTEM" (made by Hosekawa Micron K.K. ~~Nara Kikai Seisakusho K.K.~~) and "HYBRIDIZATION SYSTEM" (made by Nara Kikai Seisakusho K.K.) wherein toner particles are pressed against an inner wall of a casing under action of a centrifugal force exerted by blades stirring at high speeds, thereby applying mechanical impact forces including compression and abrasion forces to the toner particles.--

Please amend the specification at page 87, lines 4-10 to read as follows:

--The inorganic fine powder having a number-average primary particle size of 4 - 80 nm may preferably have a specific surface area of 20 - 250 m²/g, more preferably 40 - 200 m²/g; as measured by the nitrogen adsorption BET method, e.g., the BET multi-point method using a specific surface area meter ("~~Autosorb~~ AUTOSORB 1", made by Yuasa Ionix K.K.).--

Please amend the specification at page 91, line 11 to page 92, line 9 to read as follows:

--Further, if the volume-average particle size is larger than the above-mentioned range, the number of electroconductive fine powder particles per unit weight is reduced, so that it becomes difficult to sufficiently attain the effect of promoting the recovery of the transfer-residual toner particles. Further, because of the decrease in number of the electroconductive fine powder particles, in view of the decrease and deterioration of the electroconductive fine powder at a vicinity of the charging member, it becomes necessary to increase the content of the electroconductive fine powder in the developer in order to continually supply the electroconductive fine powder to the charging section and stabilize the uniform chargeability of the image-bearing member ensured by intimate contact via the electroconductive fine powder between the image-bearing member and the contact charging member. However, if the content of the electroconductive fine powder is excessively increased, the developer as a whole is liable to have a lower chargeability and developing performance, thus causing image density lowering and toner scattering, especially in a high humidity environment. From these viewpoints, it is further preferred that the volume-average particle size of the ~~developer~~ electroconductive fine powder is 5 μm or smaller.--

Please amend the specification on page 108, line 6 to page 109, line 11 to read as follows:

--The particle size distributions and average particle sizes may be measured by using, e.g., Coulter Counter Model TA-II or ~~Coulter~~ COULTER MULTISIZER (respectively available from Coulter Electronics, Inc.). Herein, these values are determined

based on values measured by using ~~Coulter~~ COULTER MULTISIZER connected to an interface (made by Nikkaki K.K.) and a personal computer ("PC9801", made by NEC K.K.) for providing a number-basis distribution and a volume-basis distribution in the following manner. A 1%-aqueous solution is prepared as an electrolytic solution by using a reagent-grade sodium chloride (it is also possible to use ISOTON R-II (available from Coulter Scientific Japan K.K.)). For the measurement, 0.1 to 5 ml of a surfactant, preferably a solution of an alkylbenzenesulfonic acid salt, is added to a dispersant into 100 to 150 ml of the electrolytic solution, and 2-20 mg of a sample toner is added thereto. The resultant dispersion of the sample in the electrolytic solution is subjected to a dispersion treatment for ca. 1-3 minutes by means of an ultrasonic disperser, and then subjected to measurement of particle size distribution in the range of 2.00 - 40.30 μm divided into 13 channels by using the above-mentioned Coulter counter with a 100 μm - aperture to obtain a volume-basis distribution and a number-basis distribution. From the volume-basis distribution, a weight-average particle size (D4) and a volume-average particle size (Dv) are calculated by using a central value as a representative value channel. From the number-basis distribution, a number-average particle size (D1) and a number-basis variation coefficient (S1) is calculated.--

Please amend the specification on page 133, line 26 to page 134, lines 5 to read as follows:

--The classification method and apparatus used for production of magnetic particles are not particularly limited. In order to obtain a desired particle size efficiently, it

is preferred use a sloped inertia classifier such as “ELBOW JET”, a centrifugal separator, such as “DISPERSION SEPARATOR” or “~~Turboplex~~” “TURBOPLEX”, or sieving.--

Please amend the specification on page 188, lines 7-22 to read as follows:

--The thus-formed polymerizate monomer mixture was charged into the above-prepared aqueous medium and stirred at 60°C in an N₂ atmosphere for 15 min. at 10,000 rpm by a TK ~~homomixer~~ HOMOMIXER (made by Tokushu Kika Kogyo K.K.) to disperse the droplets of the monomer mixture. Then, the system was further stirred by a paddle stirrer and subjected to 6 hours of reaction at 60°C. Thereafter, the liquid temperature was raised to 80°C for further 4 hours of reaction. After the reaction, the system was subjected to 2 hours of distillation at 80°C. After cooling, hydrochloric acid was added to the suspension liquid to dissolve the calcium phosphate salt. Then, the polymerizate was filtered out, washed with water and dried to recover black-colored Magnetic toner particles 1 having a weight-average particle size (D₄) of 7.1 μm.--

Please amend the specification on page 191, line 26 to page 192, line 14 as follows:

--The above ingredients were blended in a blender and melt-kneaded by a twin-screw extruder heated at 105°C. After being cooled, the kneaded product was coarsely crushed by a hammer mill and finely pulverized by a jet mill, followed by pneumatic classification. The classified pulverizate was surface-treated by an impact-type surface treatment apparatus under the conditions of treatment temperature of 50°C and a

rotor blade peripheral speed of 90 m/sec to obtain spherical Magnetic toner particles 13 of $D_4 = 9.3 \mu\text{m}$. Then, 100 wt. parts of Magnetic toner particles 13 were blended with 1.2 wt. parts of the hydrophobic silica fine powder used in Magnetic toner 1 and 1.6 wt parts by Electroconductive fine powder 3 by a ~~Henschel~~ HENSCHEL mixer to obtain Magnetic toner 13.--

Please amend the specification at page 192, lines 16-23 to read as follows:

--Sphered Magnetic toner particles 14 of $D_4 = 8.6 \mu\text{m}$ were prepared similarly as Magnetic toner particles 13 except for pulverizing the coarsely crushed product by means of a ~~turbo mill~~ TURBO MILL (made by Turbo Kogyo K.K.), followed by treatment by an impact-type surface treating apparatus (treatment temperature = 50°C , rotating blade peripheral speed = 90 m/sec).--